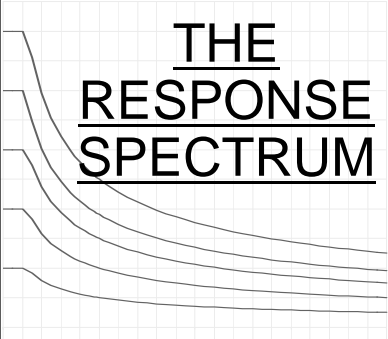


The Canadian Society for Civil Engineering, Vancouver Section






THE RESPONSE SPECTRUM

**Response Spectrum Analyses Case
Studies, Applications to Bridges**

Don Kennedy, M.Eng., P.Eng.
Manager, Bridge Engineering
Associated Engineering

*A Technical Seminar on the Development
and Application of the Response Spectrum
Method for Seismic Design of Structures*



1-2 June 2007 Vancouver, BC

Outline 2

Four Case Studies:

1. Application of RSA to bridge seismic design
2. Mission Bridge – Comparison of demands from RSA and time history analyses
3. Lake City Overpass: RSA demands and combinations
4. Knight Street Bridge retrofit – RSA and modeling

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Outline

3

Four Case Studies:

1. **Application of RSA to bridge seismic design**
2. Mission Bridge – Comparison of demands from RSA and time history analyses
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4. Knight Street Bridge retrofit – RSA and modeling

Implications of design forces on columns

4



Implications of design forces on columns

5



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Implications of design forces on columns

6



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Implications of design forces on columns
(Too much strength?)

7



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Implications of design forces on columns
(Too little strength, little ductility (old codes))

8



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Implications of design forces on columns

9



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Implications of design forces on columns

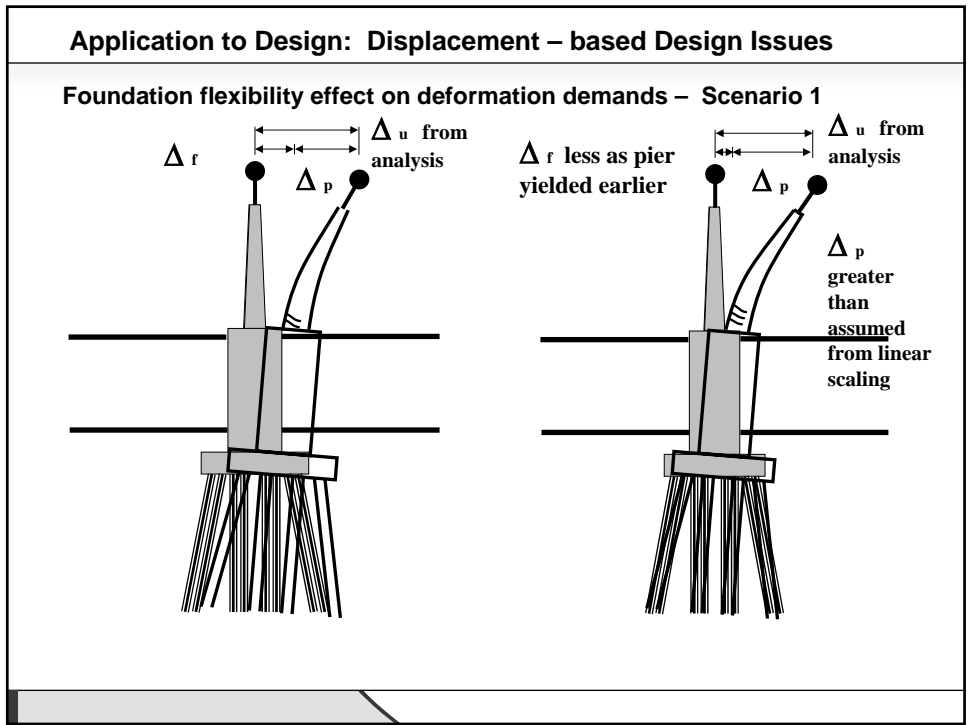
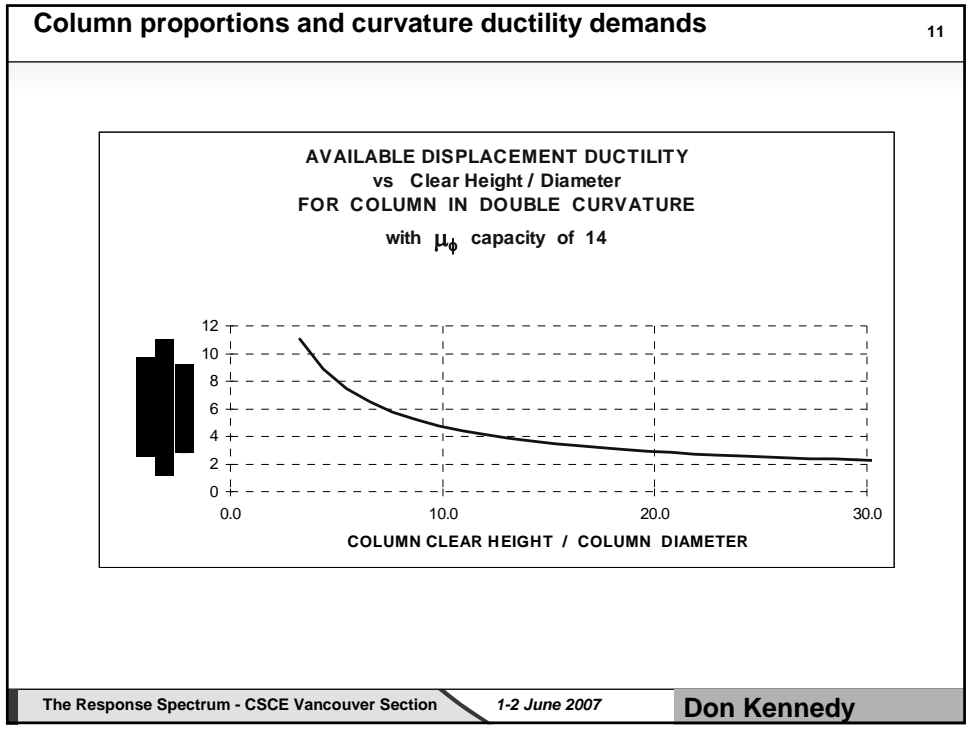
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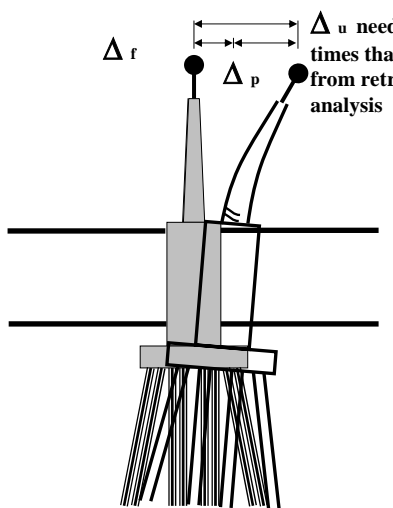
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Foundation flexibility - Scenario 2 : Design Criteria requires $1.5 \times D_{analysis}$



Δ_f

Δ_p

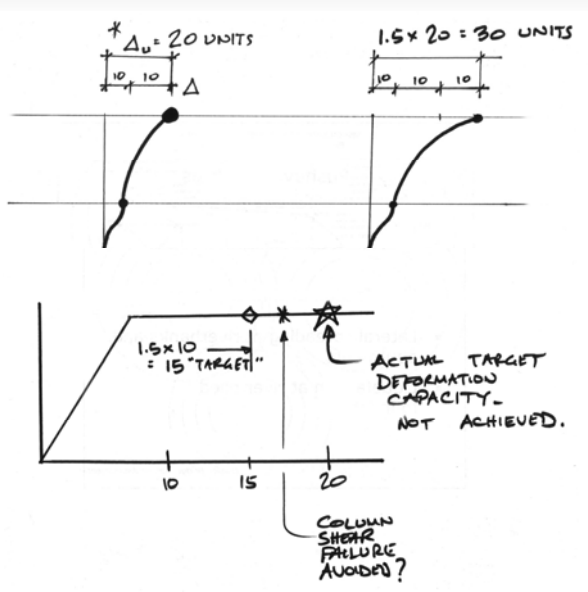
Δ_u need 1.5 times that from retrofit analysis

Criteria may require capacity of 150% of the ultimate displacement – not merely of the pier’s mechanism displacement from pushover analysis.

If retrofit is designed to achieve a target mechanism displacement, prior to (say) a column shear failure, the criteria may not have been met.

This criteria may be very difficult to achieve if foundation flexibility contributes significantly to drifts. Consider alternative retrofit (e.g. pile hinging)

Foundation flexibility - Scenario 2 : Design Criteria requires $1.5 \times D_{analysis}$



* $\Delta_u = 20$ UNITS

$1.5 \times 20 = 30$ UNITS

1.5 x 10 = 15 "TARGET"

ACTUAL TARGET DEFORMATION CAPACITY NOT ACHIEVED.

COLUMN SHEAR FAILURE AVOIDED?

Outline

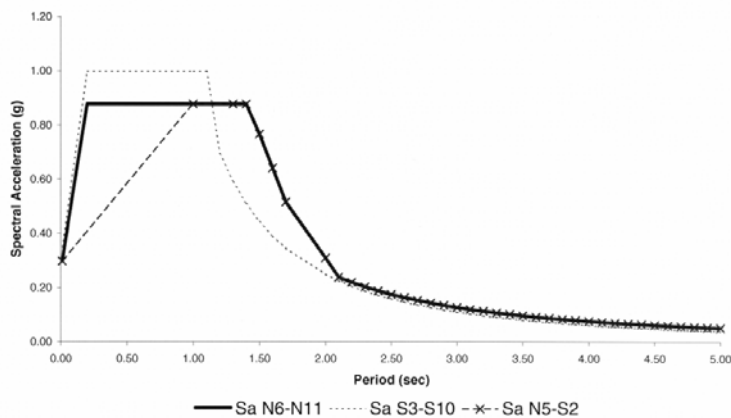
15

Four Case Studies:

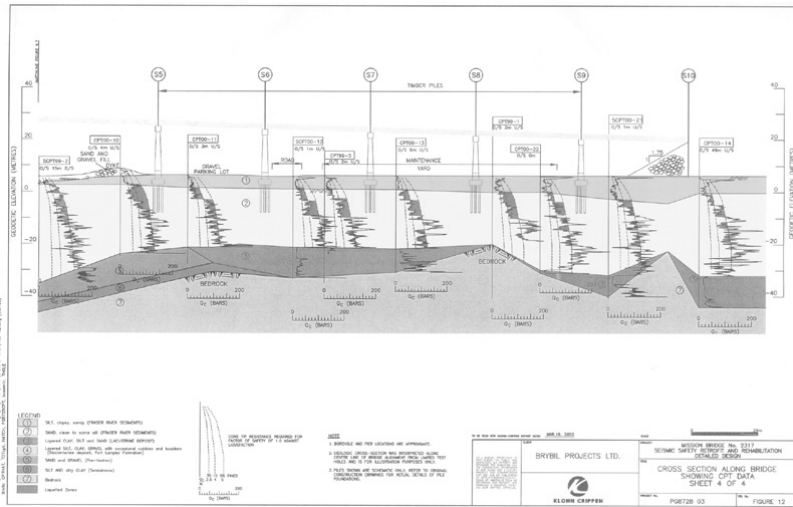
1. Application of RSA to bridge seismic design
2. **Mission Bridge – Comparison of demands from RSA and time history analyses**
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Acceleration Response Spectra

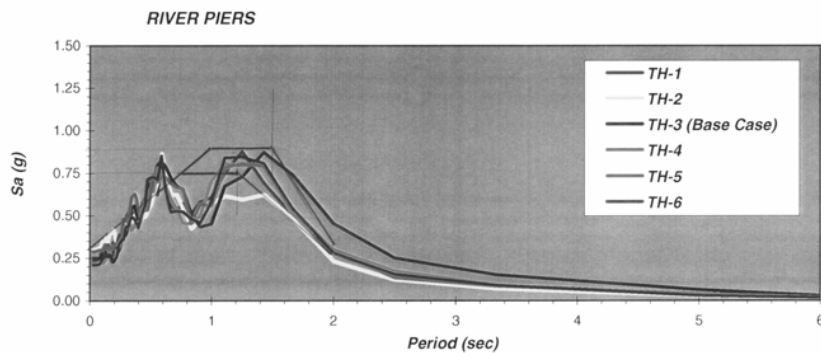
Mission Bridge Seismic Assessment
Smoothed Design Acceleration Spectra



Site variation




Acceleration Response Spectra



Modeling 19

- Idealization of the real structure
- **The continuum...**
↳ is replaced by discrete joints and elements

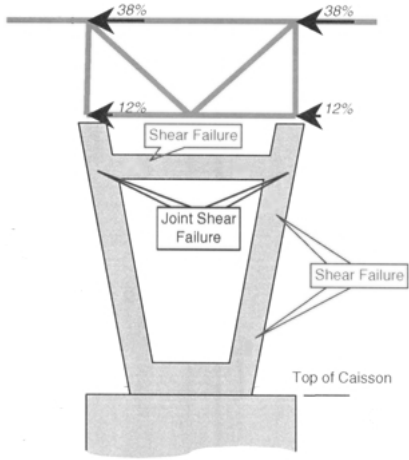


The image shows a photograph of a bridge with a trapezoidal pier. To the right of the photograph is a schematic diagram of the pier's structural model, showing a trapezoidal shape with a vertical column at the base and a horizontal top section. The diagram illustrates how the continuous structure is idealized into discrete joints and elements.

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Pier modeling

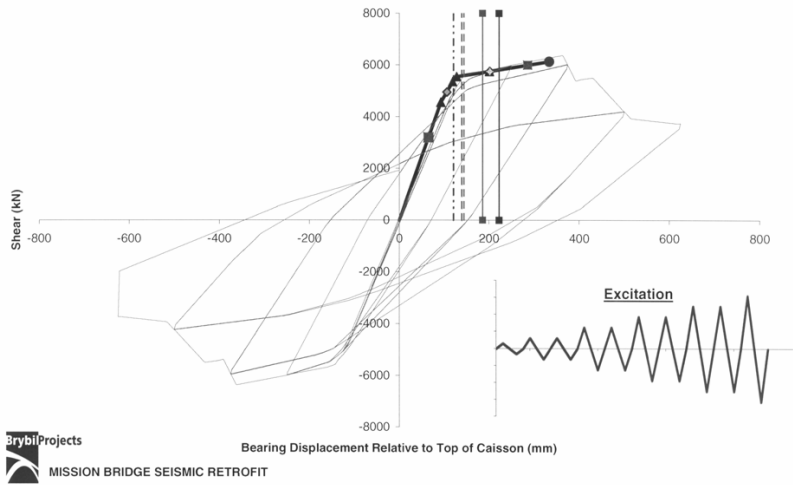
- 4 SADSAP Pivot Elements per Pier



The diagram shows a cross-section of a pier with a trapezoidal shape. At the top, there are four pivot elements. The horizontal distance between the two outer pivot elements is 38%, and the horizontal distance between the two inner pivot elements is 12%. The diagram indicates several failure modes: 'Shear Failure' at the top of the pier, 'Joint Shear Failure' at the joint between the top and the main body of the pier, and 'Shear Failure' at the base of the pier. The base of the pier is labeled 'Top of Caisson'.

Structural Analysis – Pier Nonlinearities

FIGURE 5.5 Pier N1 & S1 Transverse Pushover Response
Stiffness and Strength Degradation with Subsequent Cycles



Structural Analysis – Pier Nonlinearities

Oak Street & Quenborough Bridges - Two Column Bent Tests

35

Oak Street & Quenborough Bridges - Two Column Bent Tests

31

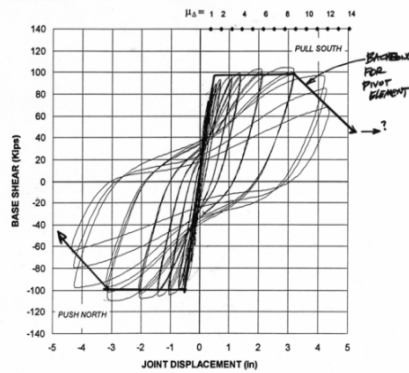


Fig. 6.4(a) Lateral Load Displacement Response for OSB4

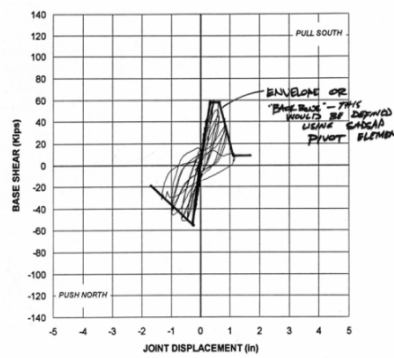
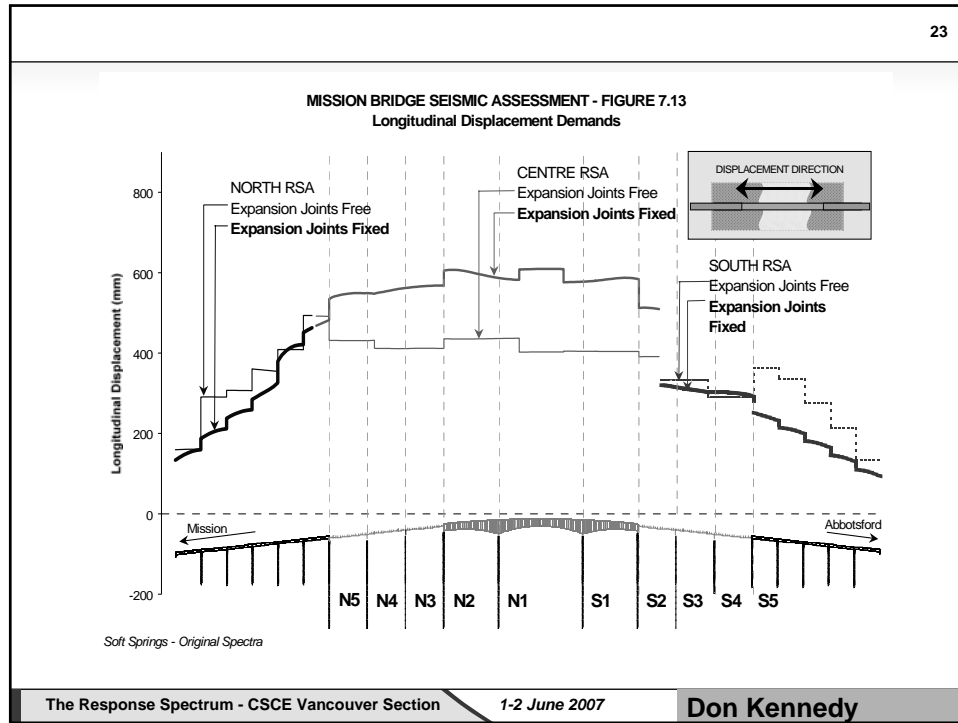


Fig. 6.1 Lateral Load Displacement Response for OSB1

AS CONSTRUCTED - NOT RETROFIT

NOTE: 1) SACSAP DOES NOT DIRECTLY ACCOUNT FOR DEGRADATION IN SUBSEQUENT CYCLES AT SAME DEFORMATION WITH STEEL BEAMS IN LATERAL RETROFIT SYSTEM.

UBC Civil Engineering - Earthquake Engineering Research Facility - Technical Report 95-02 July 1995



Structural Analysis – Model Calibration

- *Cracked Pier Stiffness Properties*
 - SAP 2000: $I_e/I_g = 35\%$
 - SADSAP: $I_e/I_g = 25\%$
- *Directional Effects*
 - SAP2000: SRSS combination
 - SADSAP: simultaneous inputs in orthogonal directions

